

## 5.1 Dimensional Analysis

**Buckingham- $\Pi$  Theorem** The Buckingham- $\Pi$  theorem states that if an equation involving  $k$  variables is dimensionally homogeneous (*i.e.*, L.H.S. units = R.H.S. units),

$$u_1 = f(u_2, u_3, \dots, u_k),$$

it can be reduced to a relationship among  $(k-r)$  independent dimensionless products, where  $r$  is the minimum number of reference dimensions required to describe the variables,

$$\Pi_1 = \phi(\Pi_2, \Pi_3, \dots, \Pi_{k-r}).$$

**Variables:** Acceleration of gravity,  $g$ ; Bulk modulus,  $E_v$ ; Characteristic length,  $L$ ; Density,  $\rho$ ; Frequency of oscillating flow,  $\omega$ ; Pressure,  $p$ ; Speed of sound,  $c$ ; Surface tension,  $\sigma_s$ ; Velocity,  $U$ .

Dimensionless group	Name	Interpretation	Types of Applications
$\rho U L / \mu$	Reynolds number, Re	$\frac{\text{inertia force}}{\text{viscous force}}$	Generally of importance in all types of fluid dynamics problems
$U / \sqrt{gL}$	Froude number, Fr	$\frac{\text{inertia force}}{\text{gravitational force}}$	Flow with a free surface
$p / \rho U^2$	Euler number, Eu	$\frac{\text{pressure force}}{\text{inertia force}}$	Problems in which pressure, or pressure differences, are of interest
$U / c$	Mach number, Ma	$\frac{\text{inertia force}}{\text{compressibility force}}$	Flows in which the compressibility of the fluid is important
$\omega L / U$	Strouhal number, St	$\frac{\text{inertia(local) force}}{\text{inertia (convective) force}}$	Unsteady flow with a characteristic frequency of oscillation
$\rho U^2 L / \sigma_s$	Weber number, We	$\frac{\text{inertia force}}{\text{surface tension force}}$	Problems in which surface tension is important

Table 1: Common variables and dimensionless groups in fluid mechanics.

Parameter	Symbol	Dimensions	Parameter	Symbol	Dimensions
Acceleration	$a$	$[L^1 T^{-2}]$	Surface tension	$\sigma_s$	$[M^1 T^{-2}]$
Angle	$\theta, \phi$ , etc.	1 (none)	Velocity	$U$	$[L^1 T^{-1}]$
Density	$\rho$	$[M^1 L^{-3}]$	Viscosity	$\mu$	$[M^1 L^{-1} T^{-1}]$
Force	$F$	$[M^1 L^1 T^{-2}]$	Volume flow rate	$Q$	$[L^3 T^{-1}]$
Frequency	$f$	$[T^{-1}]$	Pressure	$p$	$[M^1 L^{-1} T^{-2}]$

Table 2: Table of parameters with symbols and primary dimensions in two columns.  $[M]$ : mass,  $[T]$ : time;  $[L]$ : length.

## 5.2 Non-Dimensional Navier-Stokes Equation

- Define the non-dimensional variables

$$\mathbf{x}^* = \frac{\mathbf{x}}{L}, \quad \mathbf{u}^* = \frac{\mathbf{u}}{U}, \quad t^* = \frac{t}{L/U}, \quad p^* = \frac{p}{P_0},$$

where  $L$ ,  $U$  are the characteristic length and velocity, respectively.

- The dimensionless Navier-Stokes momentum equation is

$$\text{Re} \left( \frac{\partial \mathbf{u}^*}{\partial t^*} + (\mathbf{u}^* \cdot \nabla^*) \mathbf{u}^* \right) = - \frac{P_0}{\frac{\mu U}{L}} \nabla^* p^* + \nabla^{*2} \mathbf{u}^*,$$

where  $P_0 = \frac{\mu U}{L} \max(1, \text{Re})$ , *i.e.*, the viscous scale ( $\text{Re} < 1$ ) or dynamic scale ( $\text{Re} > 1$ ). This formulation ensures the pressure term has the same order of magnitude as other terms, since there is no natural scaling for pressure.

- The dimensionless continuity equation is

$$\nabla^* \cdot \mathbf{u}^* = 0.$$

**Small Re flow** ( $Re \ll 1$ )  $P_0 = \mu U/L$  and the L.H.S. eliminated,

$$\cancel{Re \left( \frac{\partial \mathbf{u}^*}{\partial t^*} + (\mathbf{u}^* \cdot \nabla^*) \mathbf{u}^* \right)} = -\nabla^* p^* + \nabla^{*2} \mathbf{u}^* \implies \nabla^* p^* = \nabla^{*2} \mathbf{u}^* \iff \mu \nabla^2 \mathbf{u} = \nabla p$$

which is known as the **Stokes equation** that can be solved analytically due to its linearity.

### Governing Equation of Stokes Flow

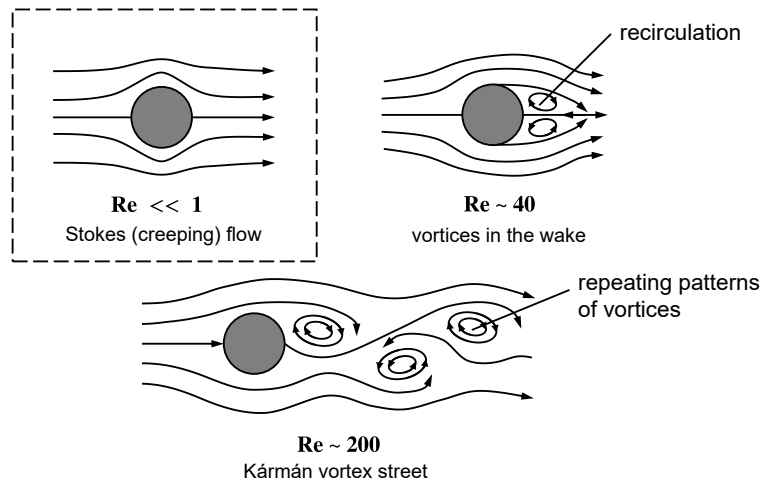
Define the vorticity as  $\boldsymbol{\omega} = \nabla \times \mathbf{u}$

$$\mu \nabla^2 \mathbf{u} = -\mu \nabla \times \boldsymbol{\omega} \quad \text{due to} \quad \nabla \times \boldsymbol{\omega} = \nabla \times (\nabla \times \mathbf{u}) = \nabla(\nabla \cdot \mathbf{u}) - \nabla^2 \mathbf{u}.$$

Further, take the curl of  $\mu \nabla^2 \mathbf{u} = \nabla p$ :

$$\begin{aligned} \underbrace{\nabla \times \nabla p}_{\text{"curl of grad is zero"}} &= \nabla \times (\mu \nabla^2 \mathbf{u}) \implies 0 = -\mu \nabla \times (\nabla \times \boldsymbol{\omega}) \\ 0 &= -\mu \left[ \underbrace{\nabla(\nabla \cdot \boldsymbol{\omega}) - \nabla^2 \boldsymbol{\omega}}_{\text{by } \nabla \times (\nabla \times \mathbf{A}) = \nabla(\nabla \cdot \mathbf{A}) - \nabla^2 \mathbf{A}} \right] \\ 0 &= -\mu \left[ \underbrace{\nabla(\nabla \cdot \nabla \times \mathbf{u})}_{\text{"div of curl is zero"}} - \nabla^2 \boldsymbol{\omega} \right]. \end{aligned}$$

The above derivation results in  $\nabla^2 \boldsymbol{\omega} = 0$ . This leads to the Laplace equation for vorticity in Stokes flow.

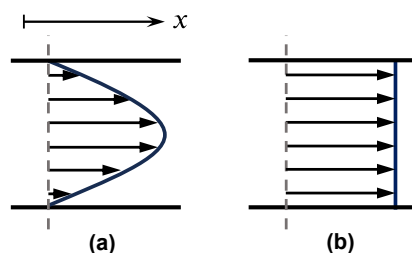


**FIG. 1:** Flow passing around a cylinder at different Reynolds numbers. The top left scenario depicts the Stokes flow when  $Re \ll 1$  - no flow separation.

**Large Re flow** ( $Re \gg 1$ )  $P_0 = \rho U^2$  and the viscous term eliminated (hence, the fluid is approximated nearly inviscid),

$$\frac{\partial \mathbf{u}^*}{\partial t^*} + (\mathbf{u}^* \cdot \nabla^*) \mathbf{u}^* = -\nabla^* p^* \implies \frac{\partial \mathbf{u}}{\partial t} + (\mathbf{u} \cdot \nabla) \mathbf{u} = -\nabla p,$$

which is known as the **Euler equation**.



**FIG. 2:** The velocity profile of flow between two parallel plates when the fluid is (a) affected by viscosity, (b) inviscid.