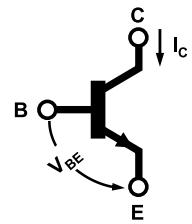


# Electrical Engineering II - Formula Summary

## 1 BJT

1. KCL

$$I_E = I_C + I_B$$



2. CCCS

$$\beta = \frac{I_C}{I_B} \quad I_C = \alpha I_E \quad (\alpha = \frac{\beta}{\beta + 1})$$

Figure 1: An n-p-n BJT

3. VCCS

$$I_C = I_S e^{\frac{V_{BE}}{V_T}}$$

In active mode: for n-p-n BJT,  $V_{BE} = 0.7V$ , for p-n-p BJT,  $V_{EB} = 0.7V$ .  $V_T \approx 25.6mV$  under room temperature.  
A modified VCCS with the early voltage is

$$I_C = I_S e^{\frac{V_{BE}}{V_T}} \left( 1 + \frac{V_{CE}}{V_A} \right)$$

with  $V_{CE,sat} \approx 0.2V$ .

4. Output resistance

$$r_o = \frac{V_A}{I_C} = \frac{\Delta v_{ce}}{\Delta i_c}$$

5. Small signal transconductance

$$g_m = \frac{I_C}{V_T} = \frac{\Delta i_c}{\Delta v_{be}}, \quad r_e = \frac{1}{g_m}$$

6. Base input resistance

$$r_\pi = \frac{\beta}{g_m} = \frac{V_T}{I_B}$$

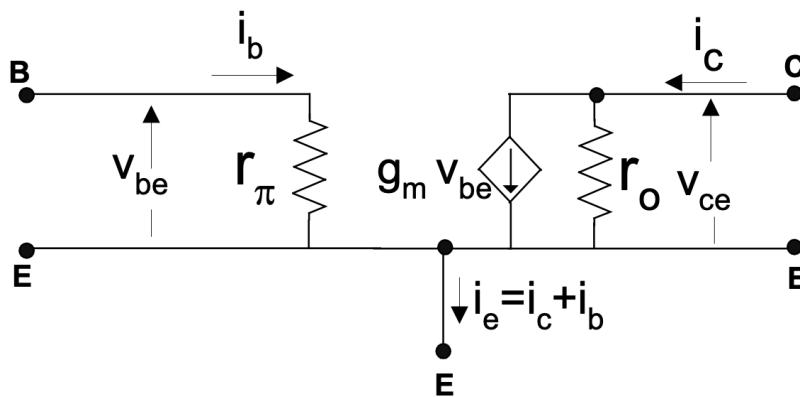


Figure 2: Small signal equivalent for BJT

## 2 MOSFET

1.  $V_{GS} > V_{TH}$ ,  $V_{DS} = 0$ , no induction current.
2. Triode region  $V_{GS} > V_{TH}$ ,  $V_{DS} < V_{GS} - V_{TH}$

$$I_D = \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH}) V_{DS}$$

3. Onset of saturation  $V_{GS} > V_{TH}$ ,  $V_{DS} = V_{GS} - V_{TH}$

$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2$$

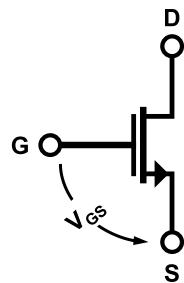


Figure 3: An n-type MOSFET

4. Saturation  $V_{GS} > V_{TH}$ ,  $V_{DS} > V_{GS} - V_{TH}$ <sup>1</sup>

$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2$$

with the channel width modulation

$$I_D = \frac{1}{2} \mu_n C_{ox} \frac{W}{L} (V_{GS} - V_{TH})^2 (1 + \lambda V_{DS})$$

where  $\lambda = \frac{1}{|V_A|}$ .

5. Output resistance

$$r_o = \frac{1}{\lambda I_D} = \frac{V_A}{I_D}$$

6. Body effect equation

$$V_{TH} = V_{TH,o} + \gamma [\sqrt{2\phi_F + V_{SB}} - \sqrt{2\phi_F}]$$

7. Small signal transconductance

$$g_m = \sqrt{2\mu_n C_{ox}} \sqrt{\frac{W}{L}} \sqrt{I_D} = \frac{2I_D}{V_{GS} - V_{TH}}$$

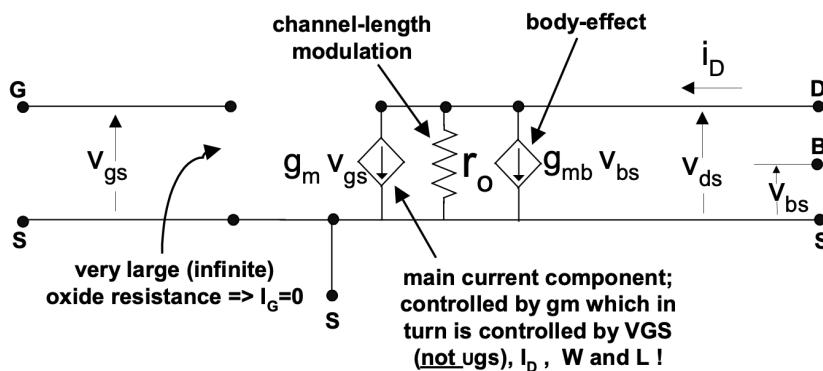


Figure 4: Small signal equivalent for MOS

## 3 Current Mirrors, Current and Voltage References

1. Simple current mirror

$$\frac{I_{out}}{I_{in}} = \frac{1}{1 + 2/\beta} \quad \frac{I_{out}}{I_{in'}} = \frac{1 + \frac{V_{CE,2}}{V_A}}{1 + \frac{V_{CE,1}}{V_A}}$$

2.  $\beta$ -compensated current mirror

$$\frac{I_{out}}{I_{in}} = \frac{1}{1 + 2/\beta^2}$$

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<sup>1</sup>bizarrely,  $V_{DS}$  is also documented as  $v_{DS}$ , but they are the same.

3. MOS simple current mirror

$$\frac{I_{out}}{I_{in}} = \frac{\left(\frac{W}{L}\right)_{out}[1 + \lambda v_{DS,out}]}{\left(\frac{W}{L}\right)_{in}[1 + \lambda v_{DS,in}]}$$

4.  $V_{BE}$ -based ref

$$I_{ref} = \frac{V_{EB}}{R}$$

5.  $V_T$ -based ref

$$I_{ref} = \frac{V_T}{R} \ln(\mu)$$

6.  $V_{BE}$  multiplier

$$V_{out} = kV_{BE} \frac{\left(\frac{W}{L}\right)_5}{\left(\frac{W}{L}\right)_2}$$

7.  $V_T$  multiplier

$$V_{out} = kV_T \ln(\mu)$$

8. Bandgap reference

$$\begin{aligned} \frac{\partial V_{EB}}{\partial T} &= -2.2mV/\text{°C} & \frac{\partial V_T}{\partial T} &= 0.086mV/\text{°C} \\ V_{out} &= 25.6V_T + V_{BE} & V_{BG} &= 1.21 - 1.31V \end{aligned}$$

## 4 Amplifiers

	Common Emitter	Common Emitter with Emitter Resistance
$A_V \left( \frac{V_0}{V_i} \right)$	$-\frac{R_C}{r_e}$	$\approx -\frac{R_C}{R_E + r_e}$
$A_{VS} \left( \frac{V_0}{V_S} \right)$	$\frac{R_b \parallel R_i}{R_S + (R_b \parallel R_i)} A_V$	$\frac{R_b \parallel R_i}{R_S + (R_b \parallel R_i)} A_V$
$R_i$	$\approx \beta r_e$	$\approx \beta(R_E + r_e)$
$R_{out}$	$R_C$	$R_C$

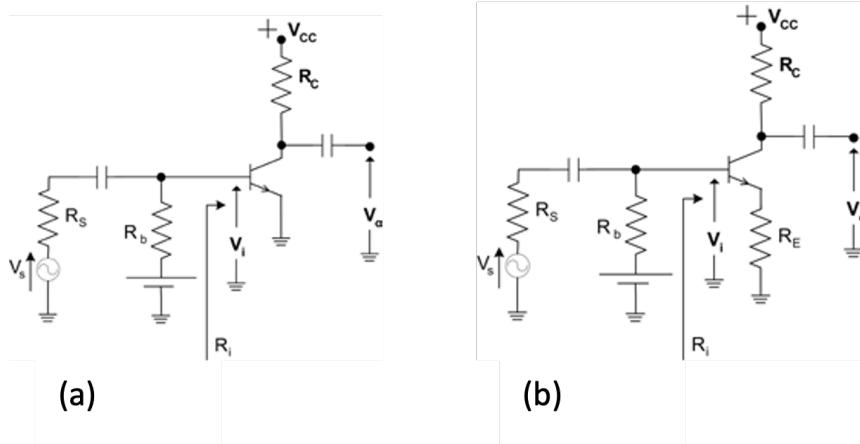


Figure 5: (a) Common emitter, (b) Common emitter with emitter resistance

- DCLL

$$I_C = -\frac{V_{CE}}{R_C} + \frac{V_{CC}}{R_C}$$

- ACCLL

$$i_c = -\frac{V_{CE}}{R_C \parallel R_L} + \frac{V_{CC}}{R_C \parallel R_L} - \frac{R_C}{R_L} I_C$$

- Optimal,  $Q$

$$I_{CQ^*} = \frac{1}{R_C \parallel R_L} \frac{R_L}{R_C + 2R_L} V_{CC}$$

$$V_{CEQ^*} = \frac{R_L}{R_C + 2R_L} V_{CC}$$

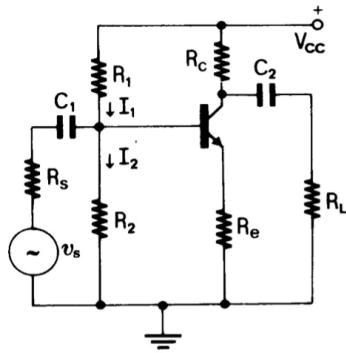
- Intersection of ACCLL and biasing line

$$V_{CE} = V_{CC} - R_C I_{CQ}$$

- Emitter degenerated ACCLL

$$i_c = -\frac{V_{CE}}{R_e + (R_C \parallel R_L)} + \frac{V_{CC}}{R_e + (R_C \parallel R_L)} - \frac{R_C \parallel R_L}{R_e + (R_C \parallel R_L)} \frac{R_C}{R_L} I_C$$

$$I_{CQ} = \frac{1}{R_e + (R_C \parallel R_L)} V_{CEQ} \quad V_{CEQ} = \frac{R_L}{R_C + 2R_L} V_{CC}$$



- Emitter degenerated DCLL

$$I_C = -\frac{V_{CE}}{R_C + R_E} + \frac{V_{CC}}{R_C + R_E}$$